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[www.rodavigo.net](http://www.rodavigo.net)

+34 986 288118

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## DYNAMIC SEALING

 **HUTCHINSON®**  
**PAULSTRA**

# DYNAMIC SEALING

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We reserve the right to modify the design and manufacture of the products and materials described in this catalogue.

The pictures of the products are supplied for information only.

The order comprises :

- the contract signed by both parts or the purchase order and the acknowledgement of receipt.
- eventually special or specific additional conditions.
- sales general conditions available upon request are part of the order.

## I - GENERAL

### I.1 - WHAT IS A SEAL ?

An element forms a sealing function when it prevents the passage of a fluid from a one enclosure to another. Such elements are called "Seals".

If the object is to prevent the flow of a fluid from an enclosure into a neighbouring enclosure **the seal is called a single seal**. If the seal must prevent the flow of another fluid which may be in the second enclosure into the first, **the seal is called a double seal**.

If the two mechanical parts between which the leakage is likely to occur are fixed with relation to each other, **the seal is called a static seal**. If one or both of these parts is moving relative to the other, **the seal is called a dynamic seal**.

In this document, we will only be dealing with **dynamic seals**.

In practice, we only meet two sorts of relative movement, which may or may not be combined:

- linear translation (such as the sliding of a piston in a cylinder).
- rotation (the relative rotation about a common axis of a shaft in a hub or a crank case).



## I.2 - TYPES OF SEALS

Many different methods have been or are still used for sealing such as :

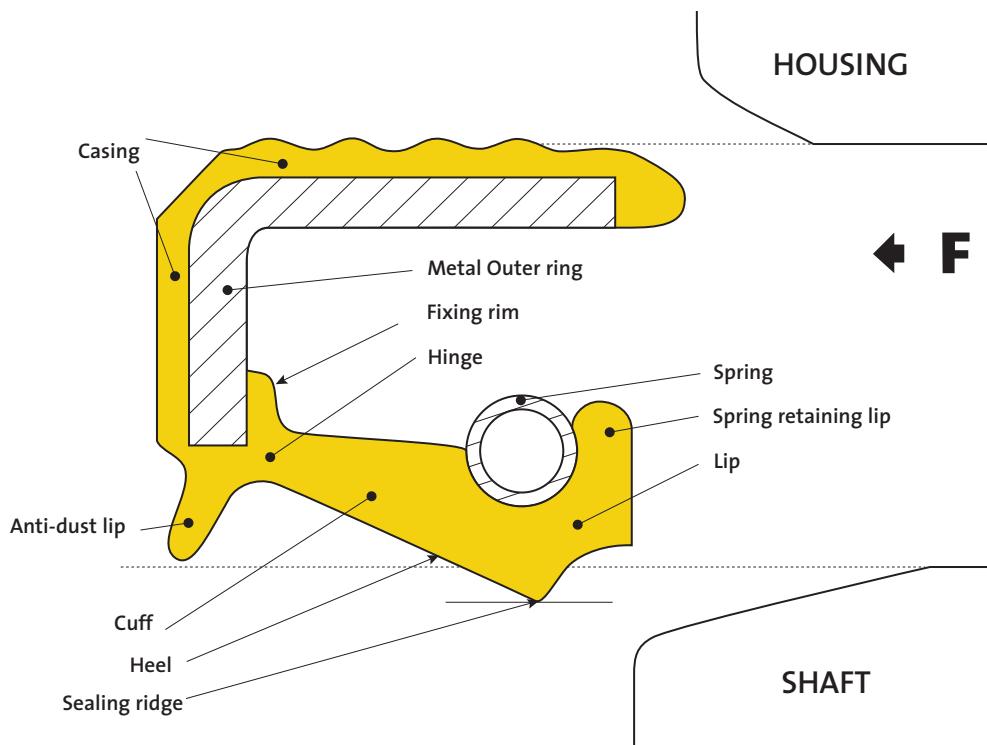
- labyrinth glands.
- stuffing-boxes.
- O-rings.
- lip seals.
- surface seals.

- **Labyrinth glands** are frictionless seals. They do not provide total sealing and do not seal if completely immersed in the fluid.
- **Stuffing-boxes** work by packing fibrous material which may or may not be braided tightly around a shaft by means of axial pressure applied by a screw cap or a flange tightened by a bolt. For many years, they have been the most common type of seals used. They produce a high frictional torque and absorb a relatively high amount of power. Although for many applications they have been replaced by lip seals or "surface" seals, they are still used a great deal, especially in the case of fluids under high pressure.
- **O-rings** are rings of synthetic elastomer of various cross-sections, most often circular (hence the name) but sometimes in the form of an X or a cross. They are most often used for static seals but can also be used in some cases as seals for rotating shafts, particularly at low speeds. They also give rise to a high frictional torque.
- **Lip seals for rotating shafts.** Lip seals first appeared about fifty years ago. They consisted of a leather cuff (which could be chromed) whose lip was kept in contact with the rotating shaft by an annular spring. In order to keep both the spring and the leather cuff in position, the parts were encased in a set of metallic collars and rings (normally at least three) which were crimped into each other. The external collar would usually be ground to size and "hard" mounted in a fixed hub. This type of seal was used a great deal, but its life was restricted as the leather wore out particularly in high temperatures. Nowadays, the leather has been replaced by synthetic elastomers which appeared on the market some forty years ago and gradually took over the role of the leather. The first of these elastomers to appear is today known as N.B.R. (Nitrile Butadiene Rubber) and was noted for its resistance to organic solvents, in particular liquid fuels and lubricating oils, even at high temperatures. The first seals manufactured had the same structure as the leather seal with its three crimped metal rings. The development of processes which ensure a very good bonding of N.B.R. to metal has enabled the structure of the seal to be simplified and has given it its present classic general shape. The discovery of new elastomers enables us to offer the user an increasingly varied range of seals, which are capable of solving increasingly difficult problems.



Segré's Plant (Maine-et-Loire) - ISO 9001

## I.3 - DESCRIPTION OF LIP SEALS



In outline, a seal for a rotating shaft consists of three essential parts :

- The Outer ring
- The elastomer
- The spring

- **The Outer ring** usually consists of a metal ring in stamped steel with a right-angled cross-section.

- **The elastomer** is itself made up of 3 parts :

- The casing
- The cuff
- The lip

- The casing (from the front surface to the back of the seal) is the part of the elastomer which is bonded to the Outer ring. It can cover it more or less entirely on the interior and/or the exterior.

- The cuff is cylindrical or slightly conical in shape and joins the Outer ring and the casing to the lip. It ensures a static seal and due to its elasticity - which is greater as it is longer - it allows slight movement of the lip due to movement of the shaft other than rotation.

- The lip is the element which ensures the dynamic seal by direct frictional contact with the shaft. It is made up of an annular beading including a double bevel forming a sharp ridge which is concentric with the perpendicular axis of the seal. The inclination of the surfaces of the bevel is designed to ensure the seal against leakage of a fluid situated on the side marked F.

- **The spring** is a spiral prestressed spring. It forms an annular ring. The join is usually effected by screwing into one end the conical spiral parts of the other end. The spring is fitted by light pressure into a groove in the beading of the lip.

## II - MATERIALS USED

### II.1 - ARMATURES

Standard material : sheet steel of XE quality (AFNOR standard A 36 401)  
 Special outer rings can be produced using other materials for special applications.

### II.2 - SPRINGS

Standard : Stabilised XC 70 steel  
 On request : Z10 CN 18-09 stainless steel (AFNOR standard A 35 586).

**NOTA :** All the PAULSTRA range of fluorinated elastomer seals fluorocarbon (FKM) are equipped with stainless steel springs.

### II.3 - ELASTOMERS

STANDARD MIXES	Mixes	Symbols	* Temperature range
	<b>NITRILE (acrylo-nitrile butadiene)</b>  This material is particularly resistant to the action of mineral oils and grease.  Suitable in most other cases.	NBR	- 30 °C to + 110 °C
	<b>FLUOROCARBON ELASTOMER</b>  This elastomer has the best chemical and heat resistant characteristics.  The new fluorocarbon formula offers very low abrasion and: - low shaft and lip wear. - resistance to ageing.	FKM	- 20 °C to + 200 °C

\* Temperatures on samples

## III - THE SELECTION OF A SEAL FOR A ROTATING SHAFT

### III.1 - THE TYPE OF FLUID TO BE SEALED

The fluids in contact with each face of the seal can be gases or liquids which are more or less viscous even pasty (in the case of greases). They must not have too aggressive actions on the materials which make up the seal (the outer ring, spring and elastomer).

#### III.1.1 - ARMATURE AND SPRING

The armature and spring of standard seals are steel, so they have a good resistance to all the chemical solvents which are currently used in industry with the exception of water and aqueous liquids which can cause rust and corrosion.

For any other kind of material, please consult our Technical Services.

#### III.1.2 - ELASTOMER

##### Chemical resistance

The standard seals made from a nitrile elastomer based mix have been designed to resist most current lubricating oils.

**For more aggressive fluids, a formula based on fluorinated elastomer fluorocarbon (FKM) would be more appropriate.**

FLUIDS	ELASTOMERS	
	Nitrile (NBR)	Fluoro-carbon elastomer (FKM)
Acetone	D	D
Acetic acid	A	D
10 % Hydrochloric acid	A	A
Concentrated Hydrochloric acid	D	A
20 % Nitric acid	D	A
10 % Sulphuric acid	A	A
Concentrated Sulphuric acid	D	A
Atmospheric air at 100 °C	C	A
Atmospheric air at 200 °C	D	A
Concentrated Ethyl alcohol	A	B
Methyl alcohol	A	B
Propyl alcohol	A	B
Ammonia	C	A
Benzene	D	B
Butter	A	A
Butane	A	A
Petrol	A	A
Super petrol	C	A
Chlorine	B	A
Cyclohexane	B	A
Water	A	A
Sewage	A	B
Concentrated Eau de Javel	C	A
Sea water	A	A
Freon	C	C
Freon 12	B	B
Carbonic gas	A	A
Smoke	C	A
Diesel oil	A	A
Diesel oil at 100 °C	C	A
Glycerine	A	A
Cereal oils	A	A
ASTM1 oil at 100 °C	A	A
ASTM1 oil at 150 °C	D	A
ASTM2 oil at 100 °C	A	A
ASTM2 oil at 150 °C	D	A

FLUIDS	ELASTOMERS	
	Nitrile (NBR)	Fluoro-carbon elastomer (FKM)
ASTM3 oil at 100 °C	A	A
ASTM3 oil at 150 °C	D	A
Gear oil at 100 °C	A	A
Gear oil at 130 °C	D	A
EP hypoid oil at 100 °C	A	A
EP hypoid oil at 130 °C	D	A
ATF oil at 100 °C	A	A
ATF oil at 150 °C	D	A
Mineral motor oil at 100 °C	A	A
Mineral motor oil at 150 °C	D	A
Synthetic motor oil at 100 °C	A	A
Synthetic motor oil at 150 °C	D	A
Silicone oil	A	A
Isooctane fuel (Fuel A)	A	A
Isooctane-toluene (Fuel B)	B	A
Kerosene JP 1	A	A
Milk	A	A
Antifreeze (water + glycol)	B	B
Brake fluid (Lockheed)	D	C
Brake fluid (Lockheed) at 50 °C	D	D
Ozone	D	A
Paraffin	A	A
Propane	A	A
Saline aluminium solutions	A	A
Magnesium salt solutions	A	A
Sodium chloride solutions	A	A
Soda	C	A
Toluene	C	A
Trichlorethylene	D	A

A: Good chemical resistance B: Average performance

C: Acceptable (depending on conditions of use) D: Unsuitable

\* For rotating housing applications please consult us

## Mechanical resistance

The new brown colored fluorocarbon (FKM) formula presents a very low abrasivity and :

- low shaft and lip wear
- resistance to ageing

## Heat resistance

For good performance an elastomeric seal must be used within its operating temperature range. The standard elastomeric mix is not only sensitive to high temperatures which harden it causing cracks and fissures, but also to intense cold which makes it hard and hardens it. The temperature which must be considered is that at the contact lip. It must be borne in mind that this gets much hotter than the ambient fluid, due to friction. For example, the temperature of the lip of a seal which seals the motor oil of a crankcase, where the shaft is rotating at high velocity (more than 8 m/s), can increase by about fifty degrees after a few minutes of service, whereas the oil, even next to the seal, will only warm up by a few degrees in the same period. The temperature displayed by a thermometer dipped into the crankcase oil is not therefore a determining factor.

In addition to the shaft speed, which is the most important factor, other parameters influence the heating of the lip such as the condition of the shaft surface, the tightness of the seal, the ventilation of the crankcase, and so on, so that it is very difficult to know the temperature of the lip in continuous operation.

The temperatures indicated in the table below are only valid if the fluid being sealed is not degraded at these temperatures.

**Where high temperatures exceed the values shown in the table below, use seals in fluorinated elastomer.**

Our technical services are at your disposal to reply to your questions about the properties of various mixes.

	Nitrile (NBR)	Fluoro-carbon elastomer (FKM)
Low temperature in °C (1)	- 40	- 30
Temperature in °C	Av..(2) Max (3)	Av.(2) Max (3)

Products to be sealed					
Mineral oil based	Motor oils	100	120	150	175
	Gear box oils	90	110	130	150
	Hypoid gear oils	90	110	130	150
	ATF oils	100	120	150	175
	Hydraulic oils	100	120	150	175
	EL and L diesel oils	90	100	+	
	Greases	100	120	150	175
Hydraulic liquids hard to ignite	HSB oil/water emulsion	80	100	-	
	HSC aqueous solution	80	100	-	
	HSD non-aqueous solution	--		130	150
Other products	Water	80	100	+	
	Detergents	80	100	+	
	Brake fluid	--		--	

(1) Temperature at which the seal continues to function.

(2) Average operating temperature.

(3) Maximum permissible temperature for not more than 10 hours over the life of the seal.

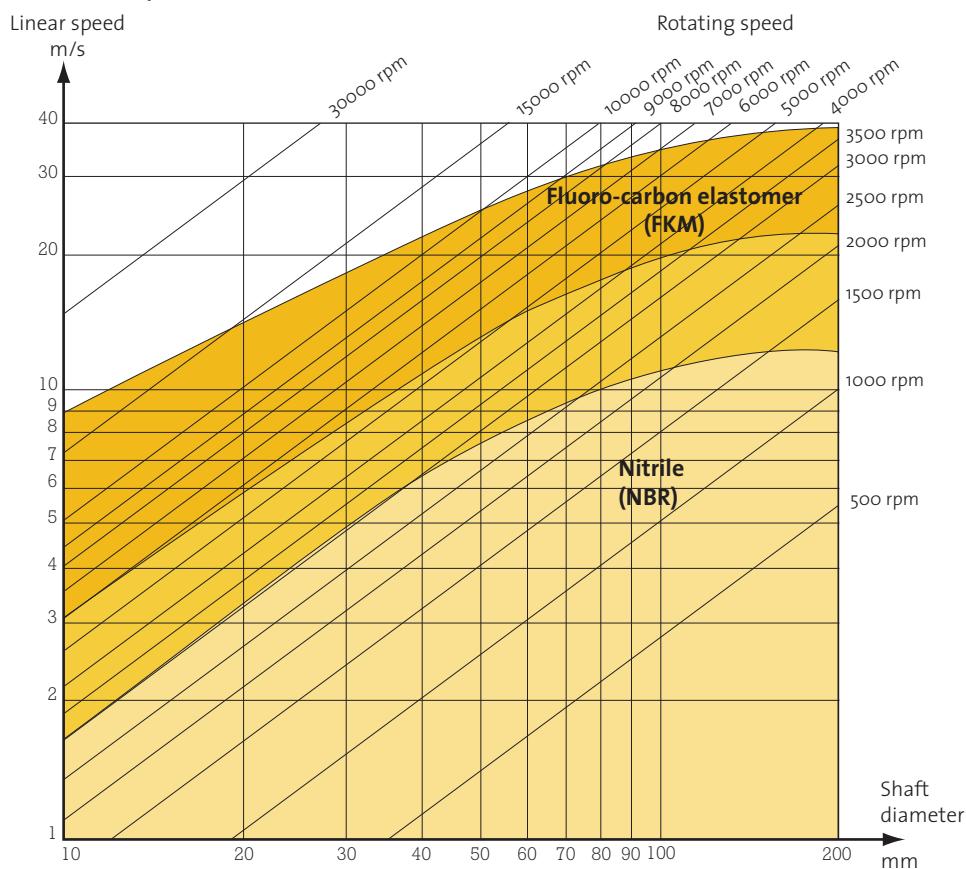
+ Resistant, but normally not used.

- Resistant, under certain conditions.

-- Does not resist.

## III.2 - SHAFT SPEED

The graph below gives an indication of the rotary or linear velocity of the shaft in relation to various elastomers which are permissible under normal conditions of use.

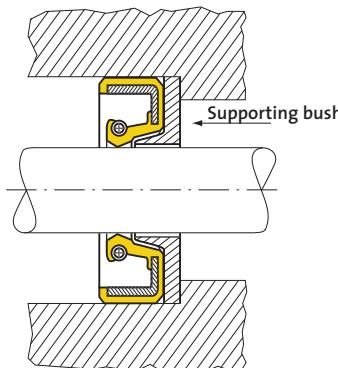


## III.3 - PRESSURE

The effective pressure to which a seal is submitted is the difference between the pressures of the fluids on each of its two sides (one of which is often the atmosphere). It is clear that the sealing lip should be found on the side which has the higher pressure. In theory, the lip seal for rotary shafts is not a pressure seal.

However, most PAULSTRA seals will resist pressures of the order of 0.5 bars without special precautions if the velocities do not exceed 3 m/s. At higher pressures, there is a risk that the lip may be turned back on itself or pressed onto the shaft with a force which gives rise to an unacceptable tightness and frictional torque. At low velocities most PAULSTRA seals will bear pressures of up to 3 or 4 bars with the addition of a supporting bush. This is not provided by PAULSTRA but it can be made up by the customer according to PAULSTRA's drawings.

The effective pressure is not necessarily constant. If the variations are slow and remain within the limits above, this is not a big problem. On the other hand, if they pulsate rapidly they can interfere with the performance of the seal.



You are advised to consult our Technical Services for any application which involves an effective pressure greater than 0.5 bars or a pulsating pressure.

## III - CONDITIONS FOR GOOD OPERATION

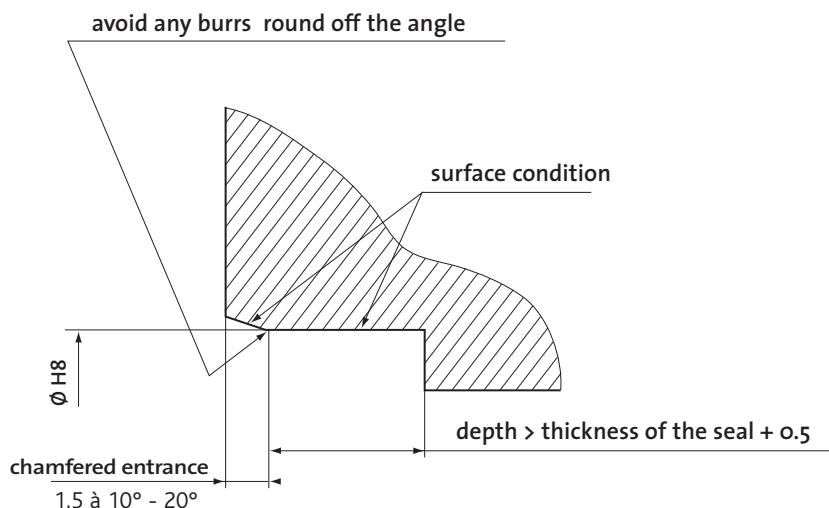
### IV.1 - THE HOUSING

**It is extremely important that there be no sharp edges.**

Our recommendations are shown on the figure below :

**Recommended shape of the housing :**

- for a covered seal :                       $R = 4 \text{ to } 12,5 \mu$   
 $Ra = 1,6 \text{ to } 4 \mu$
- for an external outer ring :               $R = 3 \text{ to } 8 \mu$   
 $Ra = 1,2 \text{ to } 2,5 \mu$



**Note : if the housing is made of a material with a high coefficient of expansion, this must be taken into consideration when defining the interference (tightness) with the seal.**

The lack of a chamfer or too small a chamfer can cause :

- A deterioration of the exterior of the seals (cutting of the elastomer or stripping of the sealing lacquer).
- A big increase in the force of insertion which could cause deformation of the outer ring.
- A defective axial positioning.

A surface with a very rough finish can cause the same problems and can therefore also be the reason for a leak. On the other hand, if the finish is too smooth the extraction force may be too low.

## IV.2 - THE SHAFT

The PAULSTRA recommendations are as follows :

- **Tolerance on the diameter** : h 11.
- **Surface state** :  $R = 0.4$  to  $1.2 ED$  (so  $Ra \approx 0.2$  to  $0.5$ ).
- **Hardness** : if  $V \leq 4$  m/s : 45 HRC minimum (say 455 HV or  $155 \text{ kg/mm}^2$ ).  
if  $V > 4$  m/s : 55 HRC minimum (say 625 HV or  $195 \text{ kg/mm}^2$ ).
- **Thickness of the treated zone** : 0.3 mm minimum.
- **Circularity** : 5 microns.
- **Neutrality** : All machined surfaces have grooves from the machining process. If these grooves are inclined in relation to the axis of the shaft, they form a helix which will produce a hydrodynamic action.

**The bearing surfaces of a seal must be neutral** (i.e. there must be no orientation of the machining grooves).

It is possible to orient the machine grooves deliberately to produce pumping from the exterior to the interior of the mechanism. However, **we advise against this as there will be increased wear of the seal**.

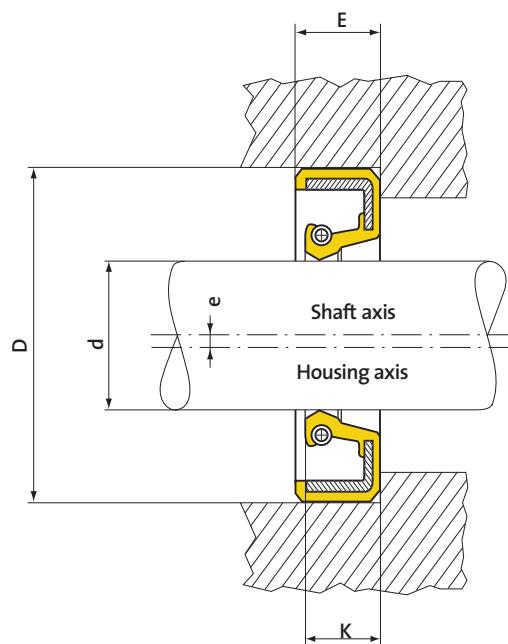
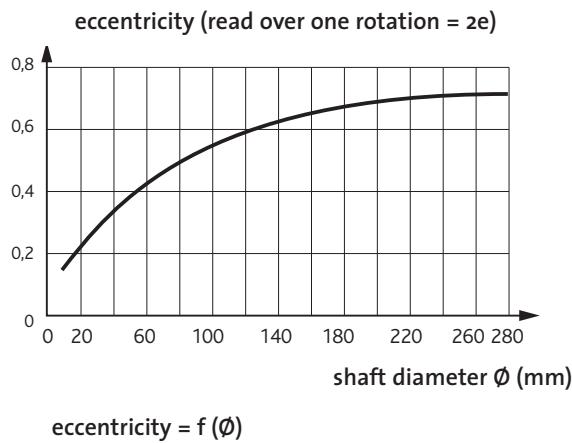
Hard chroming is also not to be recommended, unless it is of sufficient thickness and quality.

## IV.3 - ECCENTRICITY BETWEEN THE HOUSING AND THE SHAFT

The housing and the shaft should be centred on one another as precisely as possible. If there is a radial displacement between the axis of the seal and the axis of the shaft, the suppleness of the rubber lip enables assembly without "yawning" within certain limits.

The eccentricity is the distance between the axis of the seal housing and the axis of the shaft, the two axes being parallel to each other.

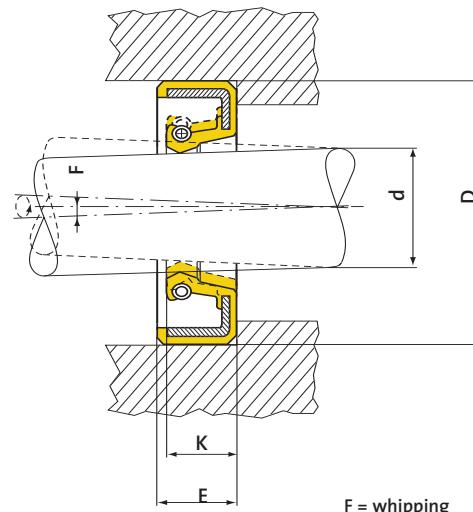
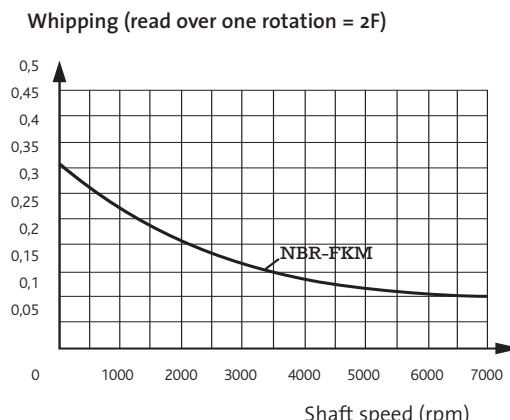
The curve below shows the maximum permitted eccentricities as a function of the shaft diameter.



## IV.4 - WHIPPING AND OUT OF TRUE

This phenomenon occurs when the geometric axis of the shaft does not coincide exactly with the rotational axis. This can be the result, for example, of a worn bearing or the bending of the shaft. The amplitude of whipping increases with distance from a bearing, so the seal should be placed as near as possible to the bearings. Whipping is measured in mm by the radius of the circle described by a point on the axis of the shaft which is in the same plane as the lip.

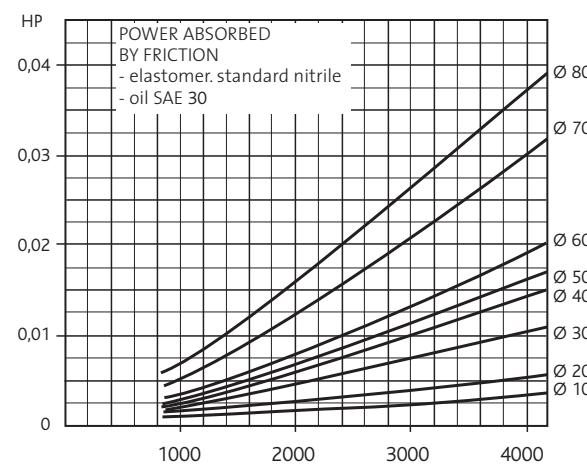
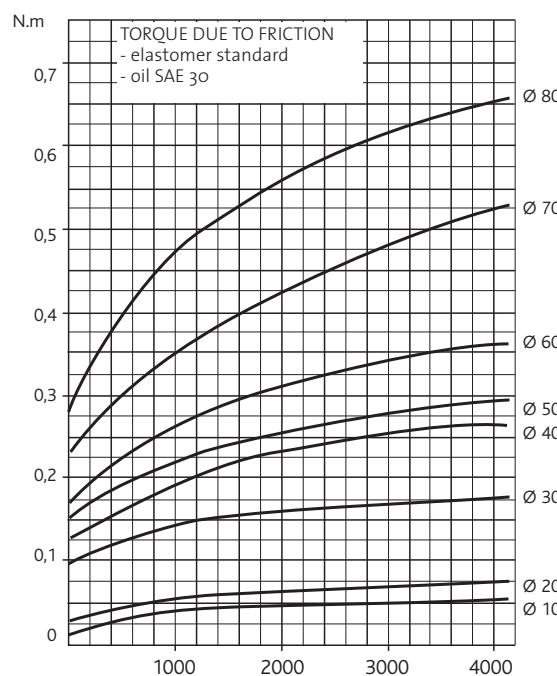
The curve below shows the maximum whipping permissible as a function of the rotational velocity of the shaft.



Whipping =  $f(V)$

## IV.5 - POWER ABSORBED DUE TO FRICTION

Due to its design, a lip seal produces friction which will provide some resistance to the rotation of the shaft. For a chosen speed, the resisting torque is function of : the shape of the seal, the friction coefficient and other environment factors such as (materials, tightness of the seal on the shaft, roughness of the shaft, wear, lubrication, temperature ...).



The curves above give a first indication for the standard Nitrile elastomer. They were plotted under average working conditions using a standard seal with little wear and a lubricated shaft with good surface finish and running temperature of less than 100 °C.

## V - THE ASSEMBLY OF SEALS

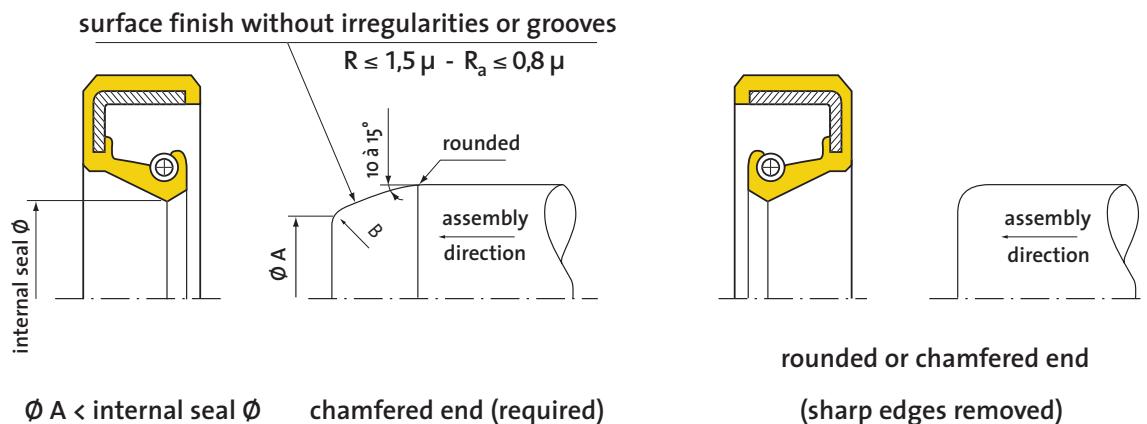
The assembly of seals is a very delicate operation which can ruin the efficiency of a very good product if it is not done properly.

The assembly of a seal must be done in accordance with the following rules :

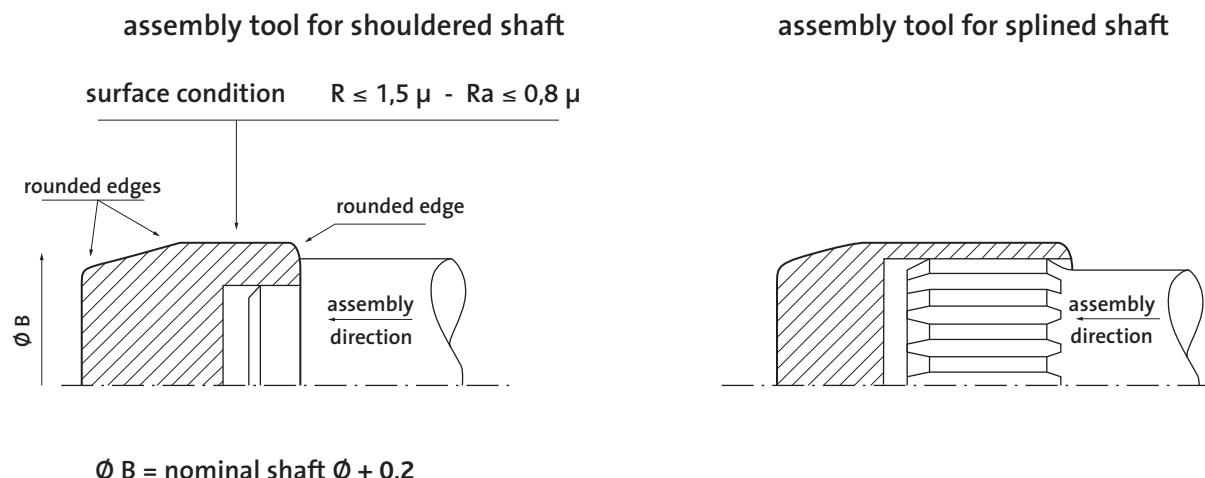
- Avoid damage to the lip.
- Avoid damage to the cover of the external diameter.
- Lubricate the sealing ridge to avoid damage at the first start-up.
- Position the seal correctly :
  - misalignment (the seal must be perpendicular in relation to the axis).
  - axial position.

The information given below should help constructors to put these rules into practice.

### V.I - ASSEMBLY ON A SHAFT WITHOUT SPLINES

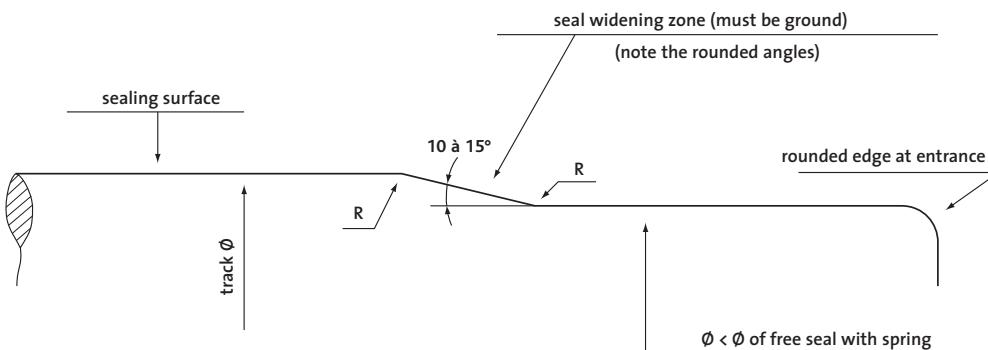


### V.2 - ASSEMBLY ON A SHAFT WITH SPLINES OR A SHOULDER



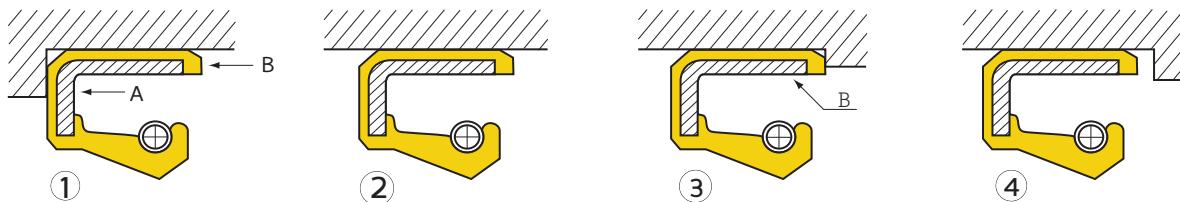
The use of these assembly tools is helpful. However, we recommend the use of a lead-in on the shaft whenever possible.

## V.3 - PAULSTRA RECOMMENDATIONS FOR THE SHAFT



Mounting sleeves are unnecessary as the shaft has a lead-in

## V.4 - AXIAL POSITIONNING AND ALIGNEMENT



① The seal is mounted against a stop on the rear side. This presents no particular problem provided that pressure is applied at "A" to insert it and not at "B".

② Here there is no axial stop. The mounting tool positions the seal both axially and perpendicularly.

③ The seal is mounted against a stop on the front side. This should be avoided as the elastomer at B could be compressed and the seal will tend to move out of position.

④ The housing has a shoulder as in ③, but the seal is positioned by the mounting tool. This case joint is preferable to case ③.

The mounting tool should be designed to position the seal correctly both axially and perpendicularly but its shape should be such as to allow deformation of the elastomer covering the outer ring towards the rear, thus avoiding cutting the covering at the time of insertion. In some cases, the bead "C" does not get cut off and sticks between the housing and the assembly mandrel in which case it is impossible to locate the seal. When the seals have an anti-dust lip, care should be taken that the mounting tools do not turn it back on itself.

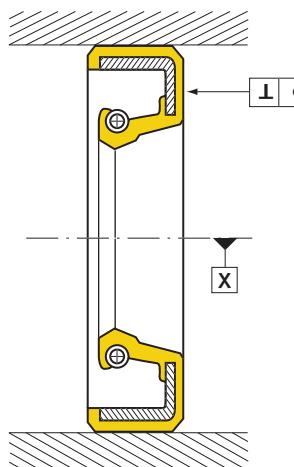
While it is true that modern seal design (corrugations on the outside, pre-centred shape chamfers without burrs, etc.) tends to reduce problems during assembly, the comments made are still worth noting.

Also, the elastomer part of a semi-covered seal behaves in the same way as a fully covered seal.

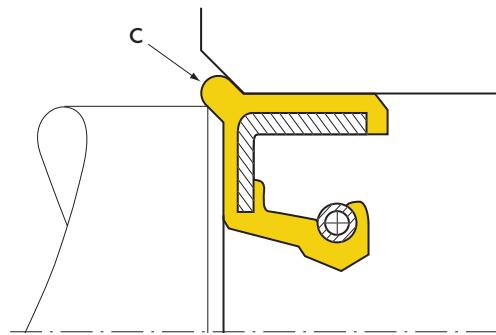
- Time should be allowed during assembly to allow in order to allow the elastomer time to settle.
- The seal must be held in position for a few seconds once mounted to avoid too large a return movement.

**We recommend the following :**

- $V = 1200 \text{ mm/mn}$  (maximum :  $1500 \text{ mm/mn}$ ).
- time held in position: 5 seconds (minimum 2 seconds).

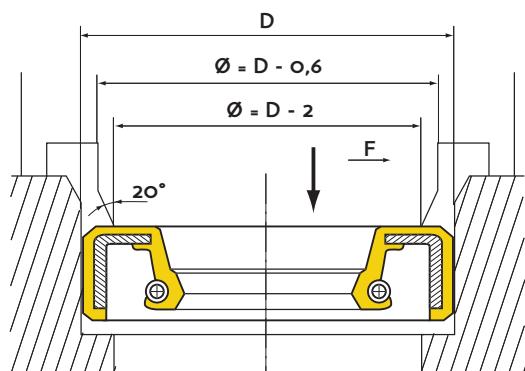


Perpendicular tolerance

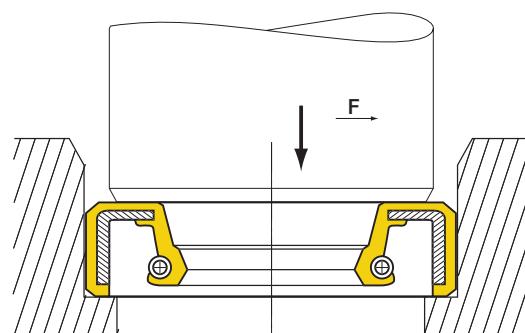


Formation of the bead

## V.5 - RECOMMENDATIONS FOR THE ASSEMBLY TOOL



GOOD



TO BE AVOIDED

## V.6 - LUBRICATION DURING ASSEMBLY

While the first means of avoiding damage to the outside of the seal is to pay attention to the housing characteristics, the second means, which is just as important, is lubrication :

- be it of the housing.
- or the outside of the seals.
- or both at the same time.

This not only avoids damage to the seal but also ensures a better axial positioning.

A seal whose outside diameter is not lubricated will certainly be damaged on the outside when it is mounted in a dry housing (elastomer cover cut or ripped sealing lacquer removed).

Also, when the unit is started up, the oil will always take some time before it reaches the lip of the seal (from a few seconds to a few tenths of seconds depending to the application).

If it is the first start, and if the lip has not been lubricated at assembly, it will function "dry" dynamically which will lead to great wear and the risk of total deterioration.

It is therefore essential to lubricate the sealing ridge.

For later starts, the problem is different because a film of oil will be retained under the lip by

capillarity action.

## V.7 - REMINDER OF THE MAIN PRINCIPLES OF ASSEMBLY

- Protect the lip and the outside of the seal by paying attention to the recommendations for the Shaft and the housing.
- Apply the insertion force to the rigid part of the outer ring.
- Centre the seal correctly in relation to the housing and/or the shaft.
- Lubricate the outside diameter and/or the housing.
- Lubricate the sealing ridge.

## V - CLASSIFICATION OF THE MAIN PROFILES OF LIP SEALS

SPRING			CORRU-GATED COVER (W)	ANTI-DUST LIP		RIDGES			
embedded (I)	visible (E)	none (O)		WITHOUT SPRING (L)	WITH SPRING (R)	on the left (G)	to the right (D)	bi-direct. (V)	
I Covered outer ring	II	IE	IO	IEW	IEL	IELR	IEG	IED	IEV
E Bare outer ring	-	EE	EO	-	EEL	EELR	EEG	EED	EEV
CS Bare outer ring reinforced	-	-	-	-	CSEL	-	-	-	-
M Semi-covered outer ring	-	ME	MO	MEW	MEWL	MEWLR	MEG	MED	MEV

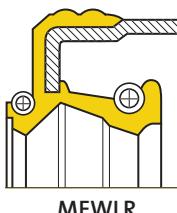
Note: other cases are available

X = exterior lip

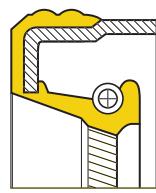
S = special cross-section

P = protector

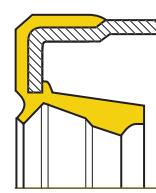
### CLASSIFICATION EXAMPLE



MEWLR



MEWG



MOWL

<b>M</b>	Semi-covered	<b>M</b>	Semi-covered	<b>M</b>	Semi-covered
<b>E</b>	Spring visible	<b>E</b>	Spring visible	<b>O</b>	No spring
<b>W</b>	With corrugations	<b>W</b>	With corrugations	<b>W</b>	With corrugations
<b>LR</b>	Anti-dust lip with spring	<b>G</b>	Ridges to the left	<b>L</b>	Anti-dust lip

















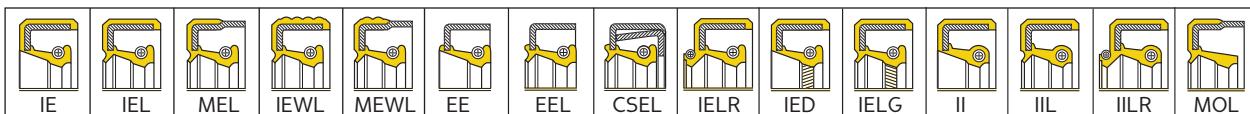












d (mm)	D (mm)	E (mm)	Type	Elastomer	Reference	d (mm)	D (mm)	E (mm)	Type	Elastomer	Reference
158	180	16	IEL	NBR	725232	195	230 230	17 17	IE II	NBR NBR	<b>722759</b> 721362
160	190	15	CSEL	NBR	<b>793135</b>	196,8	228,6	16	IEL	NBR	725019
190	15	IEL	NBR	<b>725715</b>		230	15	IE	NBR	<b>793145</b>	
190	15	IIL	NBR	724765		230	15	IE	FKM	<b>772090</b>	
190	15	IE	FKM	722313/81		230	15	IEL	NBR	<b>772090/81</b>	
165	190	13	CSEL	NBR	<b>793136</b>	205	230	16	IEL	NBR	<b>792695</b>
190	15	IE	NBR	772321		230	15	IE	NBR	<b>792811</b>	
190	15	IE	NBR	793137		230	15	IEL	NBR	<b>772091</b>	
200	15	CSEL	NBR	772084		240	15	IE	NBR	<b>79282401</b>	
200	15	IE	NBR			240	15	IEL	FKM	<b>772091/81</b>	
170	200	15	CSEL	NBR	<b>793138</b>	210	240	15	CSEL	NBR	<b>793146</b>
200	15	IE	NBR	722377		240	15	IE	NBR	<b>772091</b>	
200	15	IE	FKM	722377/81		240	15	IE	NBR	<b>772091/81</b>	
200	15	IEL	NBR	792588		250	15	CSEL	NBR	<b>793147</b>	
175	200	13	II	NBR	721122	20	250	15	IE	FKM	<b>772092/81</b>
200	13	IE	NBR	722979		250	15	IEL	NBR	<b>792696</b>	
200	15	IEL	NBR	792692		260	260	15	IE	NBR	<b>772093</b>
210	15	IE	NBR	772085		260,3	298,4	22	IEL	NBR	725009
210	15	IEL	NBR	792693		265	290	16	IE	NBR	<b>722782</b>
230	10	IIS	NBR	726200		280	320	20	IE	NBR	<b>772094</b>
177,8	209,5	16	IEL	NBR	725018	300	340	20	IE	NBR	<b>772094/81</b>
180	210	15	CSEL	NBR	<b>793139</b>	320	360	20	IE	NBR	<b>772095</b>
210	15	IE	FKM	772086/81		340	380	20	IE	NBR	772096
210	15	IEL	FKM	725655		380	420	20	IE	NBR	725009
210	15	IEL	NBR	792589		440	480	20	IE	NBR	<b>772097</b>
215	15	CSEL	NBR	793140		460	500	20	IE	NBR	772098
215	16	IE	NBR	722661		480	520	20	IE	NBR	772100
185	215	15	CSEL	NBR	<b>793141</b>						772203
215	16	IE	NBR	722863							772210
215	16	II	NBR	721280							772211
190	220	15	CSEL	NBR	<b>793142</b>						772212
220	15	IE	FKM	772088/81							772213
220	15	IE	NBR	772088							772214
220	15	IEL	NBR	792694							772215
230	16	CSEL	NBR	793143							772216
230	17	IE	NBR	722860							772217
230	17	II	NBR	721235							772218
190,5	228,6	16	IEL	NBR	725017						772219
195	230	15	CSEL	NBR	<b>793144</b>						7722112
			IE	NBR	772089						

The fluorocarbon seals previously with the suffix 83 now have the suffix 81.

Suffix 83 parts may be delivered until stocks are replaced with parts having the suffix 81.

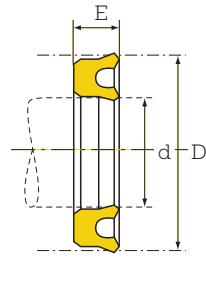
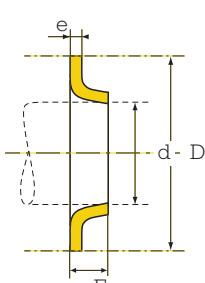
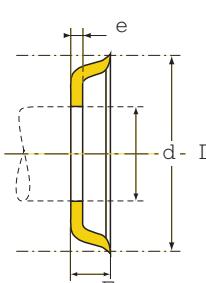
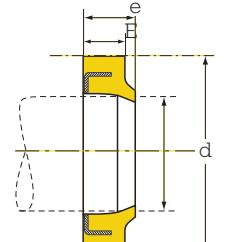
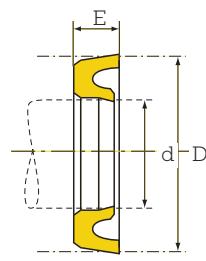
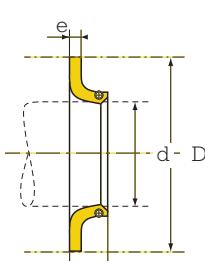
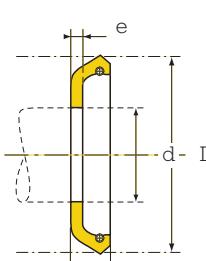
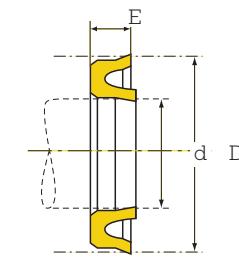
The part numbers indicated in bold type are kept in stock.

\*\*Stainless steel spring

Abbreviations : NBR = Nitrile; FKM = Fluorocarbon



# CATALOGUE OF SEALS FOR SLIDING SHAFTS


**Type DL**

**Type LIO**

**Type LEO**

**Type DRT**

**Type DLI**

**Type LIR**

**Type LER**

**Type DLE / DLES**

- Width of the groove : E + 1 mm (for DL).

- Operating parameters :

Maximum admissible pressure : 150 bars (for DL) ; 30 bars (for LIO, LEO).

Linear speed admissible : up to 0.3 m/sec depending on the operating conditions.

d (mm)	D (mm)	E (mm)	Type	Elastomer	Reference
4	14	12	DL	NBR	710093
6	14	11,5	DL	NBR	<b>710620</b>
	32	10	LEO	NBR	714057
8	14	3,5x5	DRT	NBR	711700
	14	4	DLS	NBR	716501
	17,9	5,5x1,5	LEO	NBR	714432
9	20	4	DLS	NBR	710678
10	16	3,5x5	DRT	NBR	711701
	17,9	5,5	LEO	NBR	714045
	20	7	DLP	NBR	711001
11	28	7x2,5	LIO	NBR	712094
	36	12	LEO	NBR	714020
12	18	3,5x5	DRT	NBR	711702
	22	55	DLS	NBR	710679
	22	5x1,5	DLI	NBR	716502
	22	6,5	LIO	NBR	712350
	25	DLS	NBR		710233
13	21	5x2	LIO	NBR	712414
14	20	3,5x5	DRT	NBR	711703

The part numbers indicated in bold type are kept in stock.

d (mm)	D (mm)	E (mm)	Type	Elastomer	Reference
14	26	8	LIR	NBR	713653
	38,1	10	DL	NBR	710132
15	21	3,5x5	DRT	NBR	711704
	25	8	DLT	NBR	711404
	25	10x3	LEO	NBR	<b>714178</b>
	30	10x3	LEO	NBR	<b>714179</b>
16	22	3,5x5	DRT	NBR	711705
	24	9	DL	NBR	710129
	25	6,5	DLE	NBR	716506
	26	8	DLT	NBR	711405
	28	9,6	DL	NBR	710218
	35	10	LER	NBR	715402
	35	10x3	LEO	NBR	714418
	36	8x2,5	LIO	NBR	712095
	38	12	LEO	NBR	714442
	40	10	DL	NBR	710343
	40	12x3	LEO	NBR	714864
18	28	5x7	DRT	NBR	711706
	30	8	DLES	NBR	716531
	30	10	DL	NBR	710290
	32,9	7,2	DL	NBR	710431
	36	6x2	LEO	NBR	714006
	36	7x2,5	LIO	NBR	<b>712005</b>
	38	10	LIR	NBR	713613

Abbreviations : NBR = Nitrile; FKM = Fluorocarbon



## DIMENSIONS

d (mm)	D (mm)	E (mm)	Type	Elastomer	Reference
85	95 103	7x10 13x3	DRT LIO	NBR NBR	711743 712981
86	117	14	LIR	NBR	713740
88	110	8x3,5	LIO	NBR	712430
90	130	10x4	LIO	NBR	712821
92	112	12,6	DL	NBR	710068
94	112	12	DL	NBR	710079
98	114	12	DL	NBR	<b>710724</b>
100	110 116	7x10 7	DRT LER	NBR NBR	711728 715666
104	120	11	DLE	NBR	716549
106	122	12	DL	NBR	710805

The part numbers indicated in bold type are kept in stock.

d (mm)	D (mm)	E (mm)	Type	Elastomer	Reference
110	120 126	7x10 7	DRT LER	NBR NBR	<b>711729</b> 715667
115	130,2	6,5	LEOS	NBR	714008
116	202	20	LEOS	NBR	714004
120	136	7	LER	NBR	715668
125	140	9x12	DRT	NBR	711735
130	160	18	DLP	NBR	711013
140	160 160 170	18 18 18	DL DL DLT	NBR NBR NBR	710002 710047 711433
150	209	25	LEO	NBR	714781
196	228	24	DL	NBR	710001
196,3	232	21	DL	NBR	710004
278	304,8	24	DL	NBR	710564

Abbreviations : NBR = Nitrile; FKM = Fluorocarbon





PAULSTRA  
61 rue Marius Aufan – 92309 Levallois Perret Cedex – France  
T. +33 1 40 89 53 31  
[www.paulstra-industry.fr](http://www.paulstra-industry.fr)