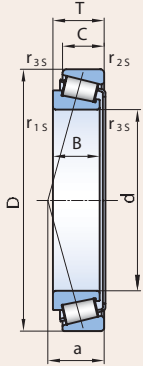




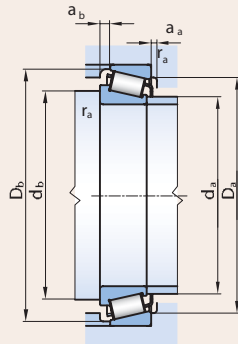
TAPERED ROLLER BEARINGS

single row

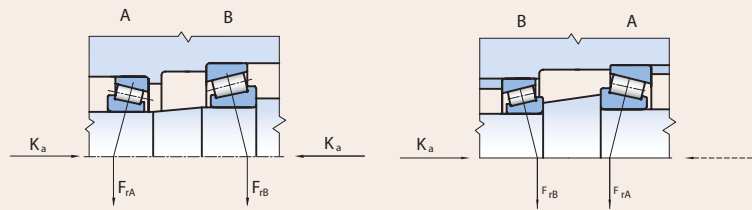


Dimensions									Basic Load Ratings		Limited Speed for Lubrication		Bearing Designation		Weight	Factors		
d	D	B	C	T	r _s	r _{2s}	r _{3s}	a	C _r	C _{or}	with		PSL	ISO	[kg]	e	Y	Y ₀
[mm]									[kN]		[min ⁻¹]		ANSI/ABMA 19.2.1)					
200.025	276.225	46.038	34.133	42.862	3.5	3.3	1	44.4	407	797	1030	1470	PSL 611-317	LM241147-LM241110	7.6	0.32	1.88	1.04
203.2	261.142	27.783	21.433	28.575	1.5	1.5	0.6	44.1	207	441	1060	1520	PSL 610-307	LL641149-LL641110	3.7	0.41	1.47	0.81
203.2	360.05	88.09	63.5	92.1	3	6	1.5	43	863	1364	900	1300	PSL 611-3		34.5	0.41	1.5	0.8
210	285	40	33	41	4	3	0.6	45.2	391	807	960	1380	PSL 611-315-2		7.3	0.32	1.88	1.04
213	285	40	33	41	4	3	0.6	45.2	391	807	960	1380	PSL 611-315-1		7	0.32	1.88	1.04
215.9	285.75	46.038	34.925	46.038	3.6	3.3	0.4	60	381	850	980	1390	PSL 611-316	LM742749-LM742710	7.8	0.48	1.25	0.69
216.5	285	40	33	41	4	3	0.6	45.2	391	807	960	1380	PSL 611-315		6.6	0.32	1.88	1.04
220	285	40	33	41	4	3	0.6	45.2	391	807	960	1380	T2DC220	T2DC220	6.3	0.32	1.88	1.04
220	300	51	39	51	3	2.5	1	59	498	1016	930	1330	32944	T3EC220	10.5	0.43	1.41	0.78
220	340	76	57	76	4	3	1	72.5	875	1587	850	1220	32044AX	T4FD220	24.1	0.43	1.39	0.77
220	265	25	19	25	2.5	1	0.4	45.6	170	425	1010	1450	PSL 610-304		2.7	0.43	1.39	0.77
228.6	295.275	31.75	23.813	33.338	3.6	3.3	0.6	15.7	258	495	930	1320	PSL 611-312	AK544090-AK544116	5	0.4	1.49	0.82
231.775	317.5	52.388	36.512	47.625	3.2	3.2	1.5	49.9	500	980	870	1250	PSL 611-302	LM245848-LM245810	11	0.32	1.87	1.03
234.95	314.325	49.212	36.512	49.212	3.6	3.3	1	57.1	479	959	880	1250	PSL 611-313	LM545849-LM545810	9.9	0.4	1.51	0.83
240	320	55	47.5	62.5	3.5	3.5	1.2	43	408	814	900	1300	PSL 611-9		12.1	0.43	1.4	0.8
240	345	60	46	60	6.4	3.3	0.4	60.1	755	1339	810	1160	PSL 611-304		16.5	0.35	1.73	0.95
247.65	304.8	22.225	15.875	22.225	1.5	1.5	1	39.3	182	356	870	1240	PSL 611-306-2	28880-28820	3.2	0.32	2.09	3.11
247.65	346.075	63.5	50.8	63.5	6.4	6.4	1.2 (2,3)	62	783	1557	800	1140	PSL 611-305	M348449-M348410	17.3	0.34	1.76	0.97
266.7	325.438	28.575	25.4	28.575	1.5	1.5	0.8	48	219	505	800	1140	PSL 611-300-1	38885-38820 class 2	5.1	0.37	1.64	0.9
266.7	355.6	57.15	44.45	57.15	3.6	3.3	1	62.2	665	1380	750	1070	PSL 611-314		15	0.36	1.67	0.92
276.225	352.425	34.925	23.812	36.512	3.6	2	1	69	340	715	740	1060	PSL 611-301	L 853049-L 853010	7.8	0.52	1.15	0.63
280	380	63.5	48	63.5	3	2.5	1	75	763	1624	700	1000	32956	T4EC280	20.3	0.43	1.39	0.76
292.1	374.65	47.625	34.925	47.625	3.3	3.3	1	65	525	1118	690	990	PSL 611-205	L 555249-L 555210	12.3	0.4	1.49	0.82
319.98	400.015	38	38	38	2	0.6	1.1x20°	115.4	328	762	630	900	PSL 612-324	GFV89X	10.2	0.83	0.72	0.4
340	460	76	57	76	4	3	1	90.5	1064	2332	550	780	32968	T4FD340	35.6	0.44	1.37	0.75
384.175	441.325	28.575	20.638	28.575	3.6	3.3	0.6	58.4	245	651	530	750	PSL 612-306	LL365348-LL365310	5.8	0.34	1.77	0.97
406.4	574.675	67.9	50.8	76.2	6.8	3.2	2	86	848	1765	470	630	PSL 612-27		53.8	0.5	1.2	0.7
409.575	546.1	87.312	68.262	87.312	6.4	6.4	1.5	104	1425	3255	430	620	PSL 612-321	M667948-M667911	53.8	0.42	1.44	0.79
409.575	546.1	87.312	68.262	87.312	6.4	6.4	0.6	109.4	1360	3230	440	620	PSL 612-329	831499	54.6	0.45	1.34	0.73
430.213	603.25	73	50.8	76.2	6.4	6.4	2	95	852	1813	450	600	PSL 612-26		58.9	0.52	1.1	0.6
440	540	40	29	46	2.5	2.5	1.1x20°	161.9	489	1103	420	600	PSL 612-323	GFV119X-129X	19.3	0.87	0.69	0.38
482.6	634.873	80.962	63.5	80.962	6.4	3.3	1.5	98.5	1473	3452	500	350	PSL 612-320	EE243190-243250	65.2	0.34	0	1.76
536.575	820	146	112	152	6	5	1.5	163	3920	7820	270	380	PSL 612-330	830238	269.9	0.43	1.39	0.77
635	933.45	177.8	141.288	179.388	11.9	6.4	5.1	165.6	5100	11650	210	300	PSL 612-328	830851	419	0.33	1.80	0.99

1) Boundary dimensions comply with the standard ANSI/ABMA 19.2. Different internal design.



Bearing Arrangement



Abutment and Fillet Dimensions

d	d _a max	d _b min	D _a min	D _a max	D _b min	a _a min	a _b min	r _a max
[mm]								
200.025	219	216	257	259	265	6	8.5	3
203.2	218	213	245	252	253	5.8	9.7	
203.2	240	230	301	328	335	10	29	2.5
210	233	236	269	270	277	8	8	2.5
213	233	236	269	270	277	8	8	2.5
215.9	227	233	260	266	279	5	8.5	3
216.5	233	236	269	270	277	8	8	2.5
220	233	236	269	270	277	8	8	2.5
220	235	232	277	288	293	9	14	2.5
220	243	234	302	326	329	12	18	3
220	228	230	252	259	259	4	6.5	1
228.6	243	242.6	280	281	287	4.7	9.8	
231.775	245	248	288	299	306	10	14	3
234.95	250	248.95	290	300.325	305	7.8	13.2	
240	253	269	286	299	311	8	15	2.5
240	255	265	317	330	355	8	13	3.5
247.65	260	258	293	296	296	8	11	1.5
247.65	263	275	318	321	336	8	13	6
266.7	281	276	311	316	317	3	8	1
266.7	284	282.7	329	339.6	347	10.1	14.6	
276.225	294	286	332	342	343	7	13	1.5
280	299	292	349	368	371	8	15	2.5
292.1	308	306	353	360	366	9	14	3
319.98	333	329.98	364	390.015	392	3.2	6.5	
340	363	354	422	446	449	15	21	3
384.175	398	400	426	429	432	4	8	3
406.4	452	459	505	533	540	10	25.5	3
409.575	437	440	502	516	534	10	15	
409.575	431	440	496	518.1	528	10	14	
430.213	476	452	530	556	565	10	25.5	6
440	459	452	503	528	531	5	16	
482.6	520	498.6	590	619	613	9.5	13.5	
536.575	578	616	724	798	777	12	36	
635	702	710	860	880	898	15	30	

Bearing Axial Load

Loading conditions	for $K_a \rightarrow$	Loading conditions	for $K_a \leftarrow$
$\frac{F_{rA}}{Y_A} \leq \frac{F_{rB}}{Y_B}$ $K_a \geq 0$	$F_{aA} = F_{aB} + K_a$ $F_{aB} = 0,5 \frac{F_{rB}}{Y_B}$	$\frac{F_{rA}}{Y_A} \geq \frac{F_{rB}}{Y_B}$ $K_a \geq 0$	$F_{aA} = 0,5 \frac{F_{rA}}{Y_A}$ $F_{aB} = F_{aA} + K_a$
$\frac{F_{rA}}{Y_A} > \frac{F_{rB}}{Y_B}$ $K_a \geq 0,5 \left[\frac{F_{rA}}{Y_A} - \frac{F_{rB}}{Y_B} \right]$	$F_{aA} = F_{aB} + K_a$ $F_{aB} = 0,5 \frac{F_{rB}}{Y_B}$	$\frac{F_{rA}}{Y_A} < \frac{F_{rB}}{Y_B}$ $K_a \geq 0,5 \left[\frac{F_{rB}}{Y_B} - \frac{F_{rA}}{Y_A} \right]$	$F_{aA} = 0,5 \frac{F_{rA}}{Y_A}$ $F_{aB} = F_{aA} + K_a$
$\frac{F_{rA}}{Y_A} > \frac{F_{rB}}{Y_B}$ 1) $K_a < 0,5 \left[\frac{F_{rA}}{Y_A} - \frac{F_{rB}}{Y_B} \right]$	$F_{aA} = 0,5 \frac{F_{rA}}{Y_A}$ $F_{aB} = F_{aA} - K_a$	$\frac{F_{rA}}{Y_A} < \frac{F_{rB}}{Y_B}$ 1) $K_a < 0,5 \left[\frac{F_{rB}}{Y_B} - \frac{F_{rA}}{Y_A} \right]$	$F_{aA} = F_{aB} - K_a$ $F_{aB} = 0,5 \frac{F_{rB}}{Y_B}$

1) Valid also for $K_a=0$